

VG H26-0068 1

# **ADVANCED MIRROR SYSTEM DEMONSTRATOR (AMSD)**

## **PROGRESS UPDATE**

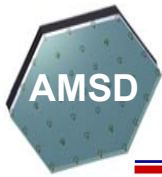
### **AT**

## **GOODRICH ELECTRO-OPTICAL SYSTEMS**

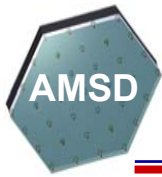
***Enrique Garcia***

Goodrich Electro-Optical Systems  
100 Wooster Heights Road  
Danbury, CT 06810

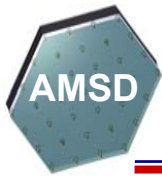
**NASA Technology Days**  
**Marshall Space Flight Center**  
**May 22-23, 2002**



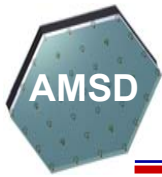
- **Program Objectives and Requirements**
- **Goodrich Configuration Overview**
- **Progress Update and Status**
  - **Facesheet**
  - **Actuators and Controller**
  - **Reaction Structure**
  - **Assembly and Integration**
- **Test Plan and Program Schedule**
- **Summary and Conclusions**



- **Program Objectives and Requirements**
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- **Diverse government applications require the benefits of:**
  - High-payoff large, light-weight mirrors
    - that advance the state of the art, and
    - are rapidly producible, and
    - are affordable
- **Specific objectives:**
  - Sub-scale demo of the mirror system technology
  - Traceable growth path to deployable, segmented optical systems
  - Provide design features that enable/improve the manufacture, integration, test, and performance of a broad range of operational systems



# Summary of Requirements and Compliance (1 of 2)

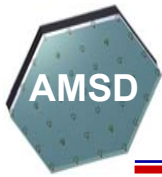


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## REQUIREMENT

## STATUS/COMMENT

- **Physical**
  - < 15 kg m<sup>-2</sup> ~ 16.7 kg m<sup>-2</sup> (actuators + CRS repair)
  - Hexagonal shape Comply (V-notch to eliminate fracture)
  - 1.2m to 1.5m point-to-point Comply (1.3 m point-to-point)
- **Mechanical**
  - Fundamental frequency traceable to full-size flight mirror system Comply
- **Ambient Environment**
  - 290K to 310K Comply
  - External mechanical disturbances Comply
- **Cryogenic Environment**
  - 30K to 55K Comply
  - No mechanical disturbances Comply
- **Survival Environment**
  - 223K to 353K 223K to 324K (limited by adhesive)
    - 25K to 353K (cryogenic)
  - 10g quasi static Comply
  - 30g vibroacoustic Comply



# Summary of Requirements and Compliance (2 of 2)

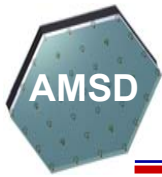


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## REQUIREMENT

## STATUS/COMMENT

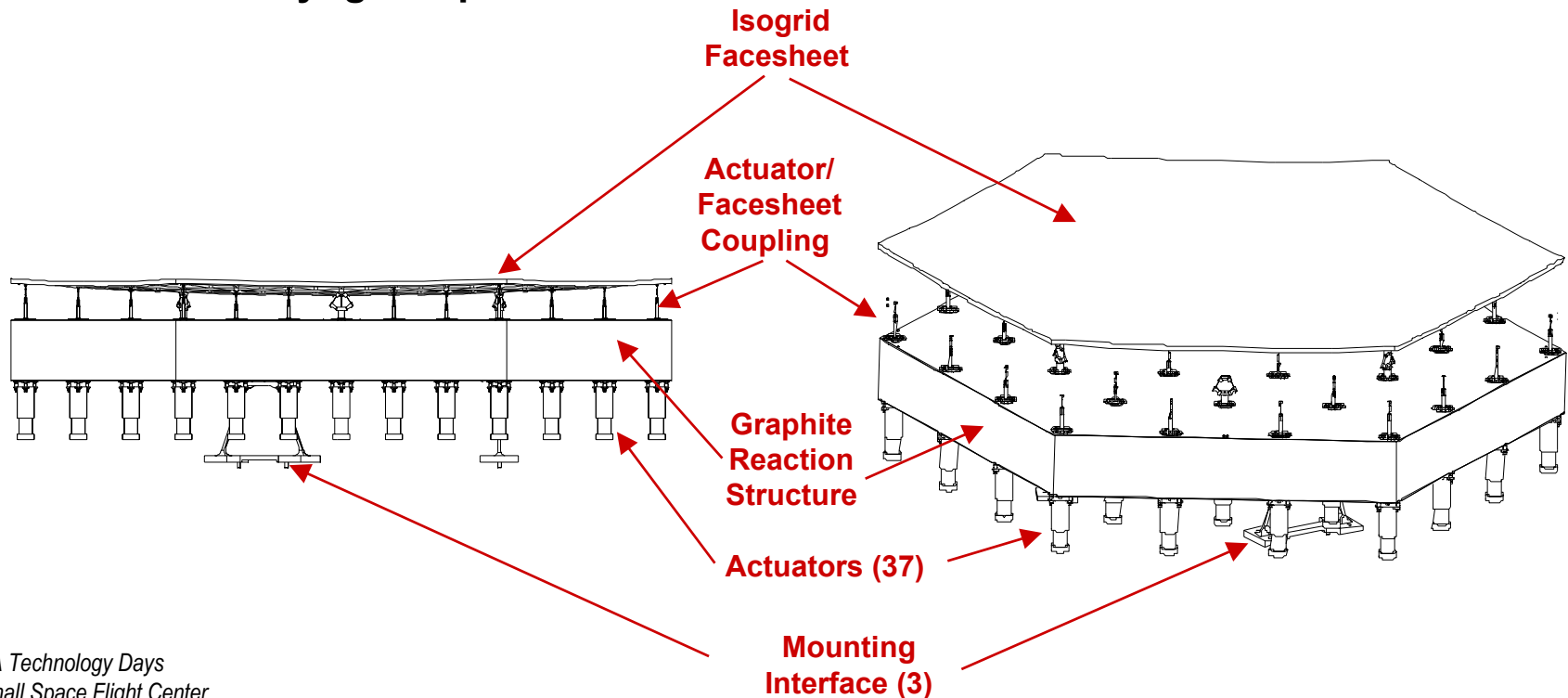
- **Total Surface Error**
  - 50 nm (rms); 250 nm (P-V) *Compliance expected*
  - Goal 25 nm (rms); 100 nm (P-V) *Achievable with additional CCP cycles*
- **Micro-roughness**
  - 40 Å (rms) *Compliance expected*
  - Goal of 20Å (rms) *Compliance expected (< 20Å typical for glass)*
  - Spatial periods 1 mm to 1 µm *Comply*
- **Prescription**
  - Off-axis parabola *Comply*
- **Vertex Radius of Curvature**
  - 10.000m ± 1mm *Comply*
- **Coating**
  - No coating required *Comply (no coating)*



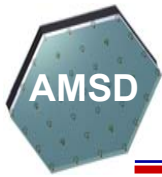
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## Architecture:

- Thin, light-weighted mirror facesheet
- Array of figure-control actuators
- Passive, stiff reaction structure
- Mirror facesheet CTE and  $\Delta L/L$  matched to reaction structure for cryogenic performance



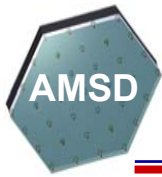




- **Figure-controlled (adaptive) mirror**
  - Reduces fabrication/test cost and schedule
  - Maximizes operational system applicability
- **Mirror facesheet CTE and  $\Delta L/L$  matched to reaction structure**
  - Enables cryogenic performance
- **Multiple material options (mirror/reaction structure pairings) from a single architecture**
- **Design optimization to mission constraints**
  - Environment
  - Performance
  - Cost
  - Schedule
  - Actuator design is common
  - Mirror facesheet and reaction structure details are material dependent
  - Traceability assessments are material dependent
    - Influenced by specific application
    - Material dependent processes and facilities



- **Cost and schedule effective optical manufacturing**
  - Non-recurring investment in tooling, followed by rapid fabrication of multiple matched facesheets
  - Work with large tools for majority of processing time
  - Actuators for low spatial frequency correction
  - Computer Controlled Polishing (CCP) for remainder
  
- **Cost and schedule effective system-level operations**
  - Actuators provide radius and figure adjustment at test and operating temperatures
  - Flexible substrate allows increased shape correction
  - Reduced reliance on ground testing

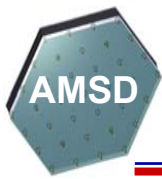


# Approach for Optical Fabrication: Stressed Mirror Polishing Overview



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- **Basic fabrication process referred to as “Stressed Mirror Polishing” (SMP)**
  - R2 (backside) of optic is fabricated to a sphere
  - Optic is held, by vacuum, against aspheric blocking body
  - Blocking body asphericity is negative of desired R1 asphericity
  - R1 is polished to a sphere
  - When vacuum is released, R1 will “spring” to desired asphere
  - Touch-up polishing after mounting to actuators
- **SMP process has several advantages**
  - Spherical fabrication process is fast, smooth, and simple
  - Minimal optic handling reduces risk - most of the time the optic is mounted to granite blocking body
  - For multiple optics of same form, investment in blocking body paid off early

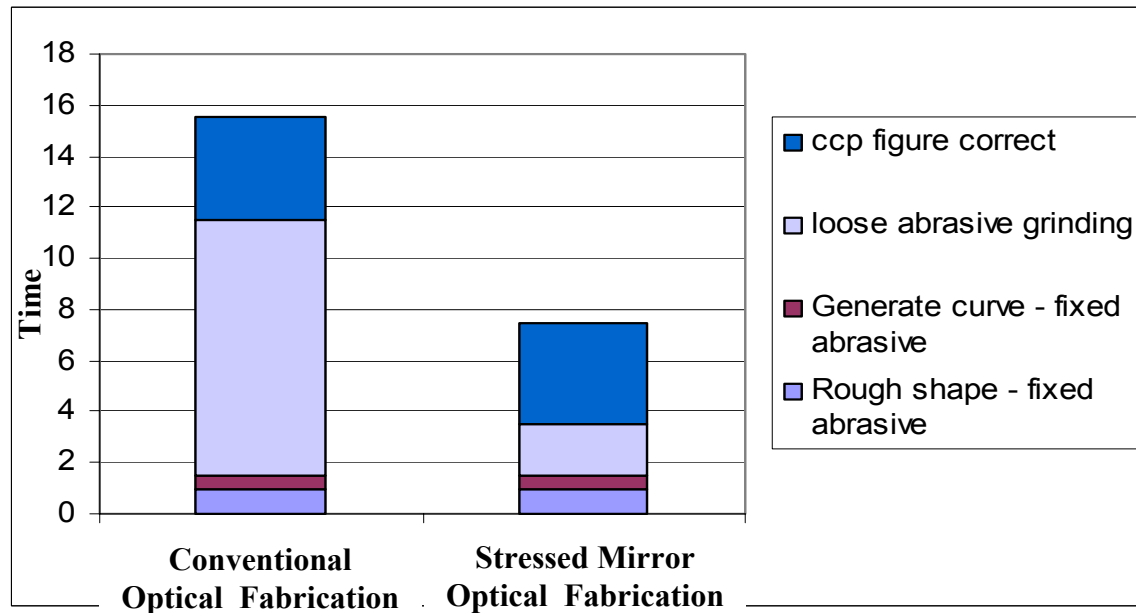


# Fabrication of Fast Aspheres by SMP

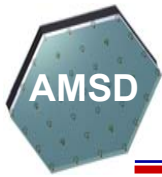


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- Taking advantage of thin section, bend the mirror to look like a sphere; grind and polish a sphere
- Large tools can remove material damage layer much faster
- Return to small-tool processing of unstressed asphere for final figure correction



***Recurring and non-recurring efforts  
tailored based on quantity of units.***



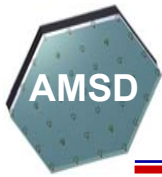
# AMSD Approach Leverages Demonstrated Large Optical Systems Technology



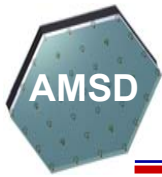
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- **HALO**
  - 3-meter diameter Primary Mirror Assembly
  - 30 kg/m<sup>2</sup>
  - tested at 100 Kelvin
- **LAMP**
  - 4-meter diameter Primary Mirror Assembly
  - room temperature High Energy Laser System
- **ALOT**
  - 4-meter diameter lightweight telescope for space operation
  - 70 kg/m<sup>2</sup> PMA
  - room temperature imaging system
- **LOS**
  - two four-meter diameter segments of 11-meter, f/1.25 primary mirror

*Large, segmented mirrors and telescopes benefiting from shape-controlled technology are demonstrated.*

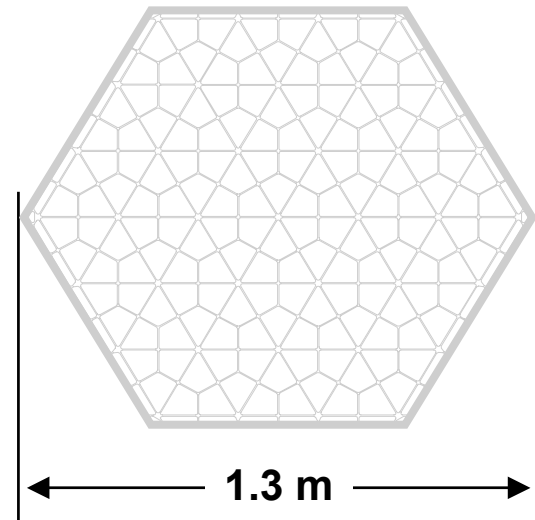


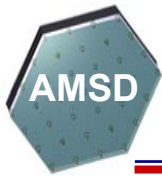
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## Light-Weighted Thin Facesheet:

- Facesheet design
- Optical fabrication (SMP)
- Light-weighting and edging
- Fracture and recovery
- Status



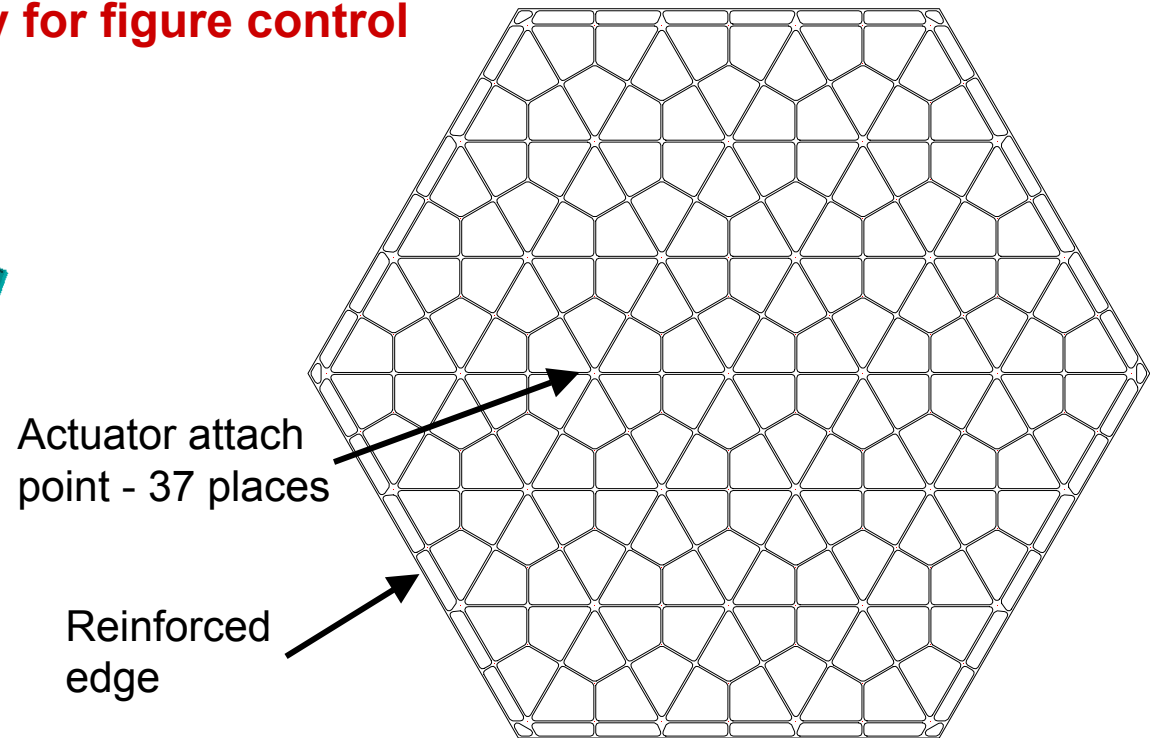
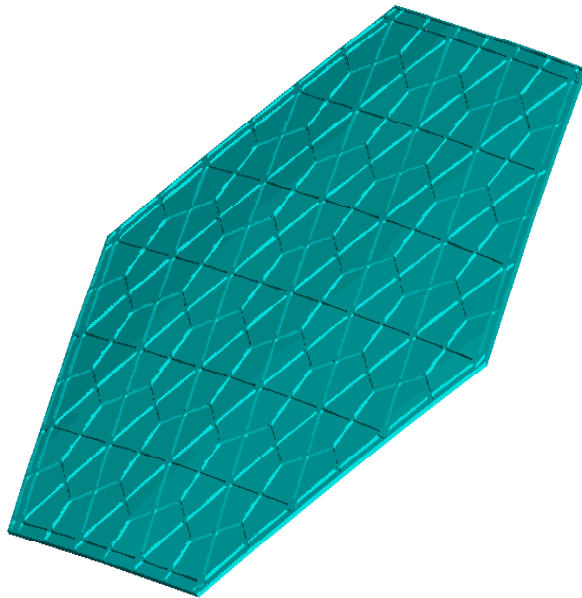


# Facesheet Design



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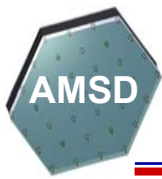
- Material is fused silica for CTE homogeneity (but could be ULE)
- Isogrid provides stiffness for 1-G support
- Isogrid provides flexibility for figure control



Typical cross-section







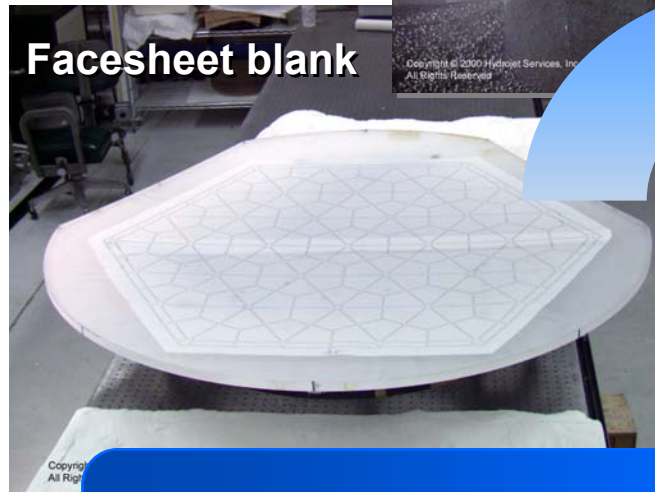
# Optical Fabrication: Preparing the Blank for Optical Finishing



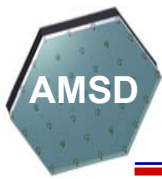
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Edged facesheet blank



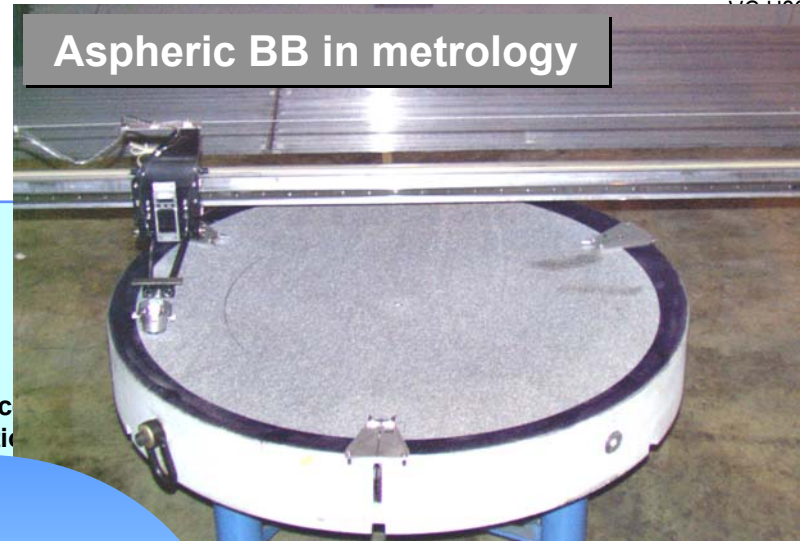
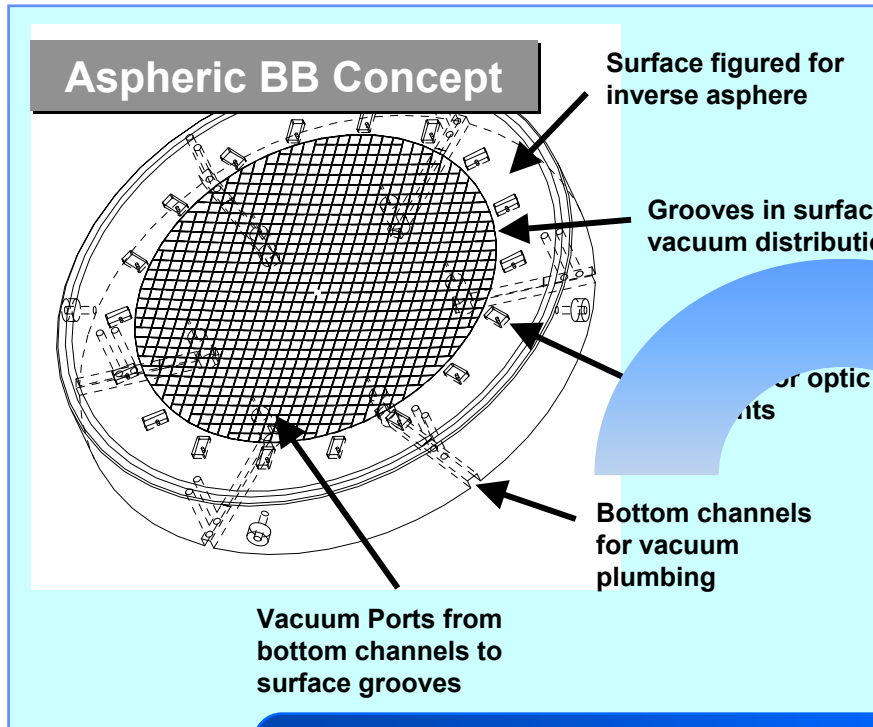
*Fused silica facesheet  
being prepared for  
optical finishing.*



# Optical Fabrication: Preparing the Aspheric blocking Body

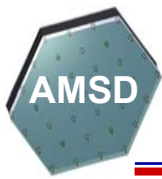


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***Fabrication of aspheric  
blocking body for SMP.***



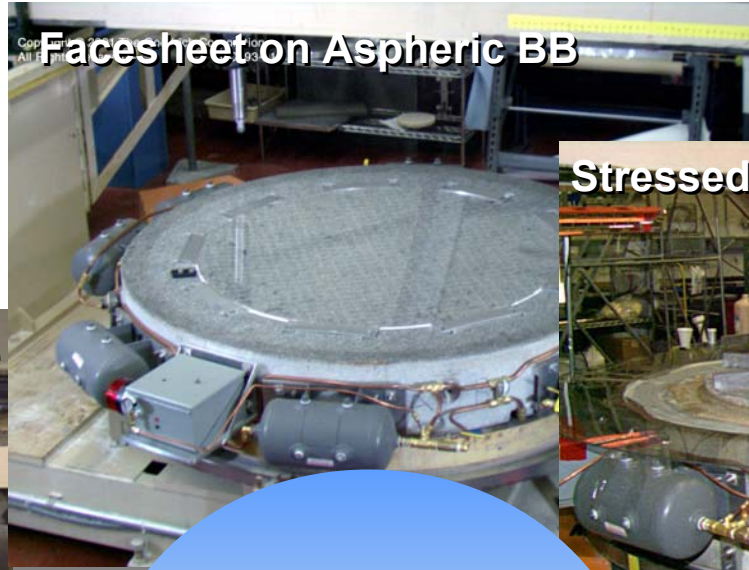


# Optical Fabrication: Optical Finishing by SMP



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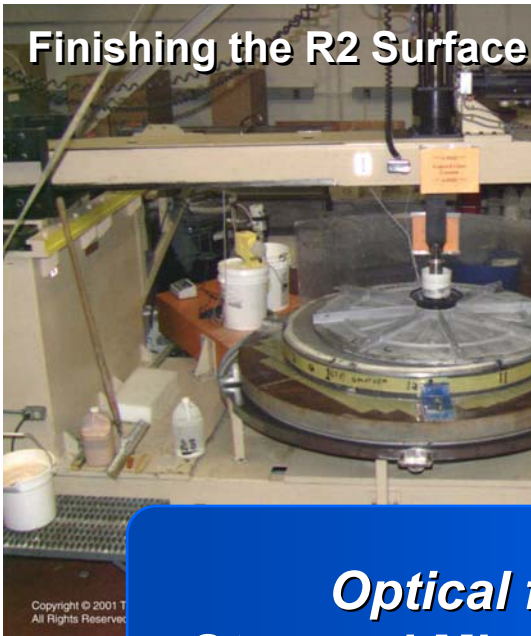
Facesheet on Aspheric BB



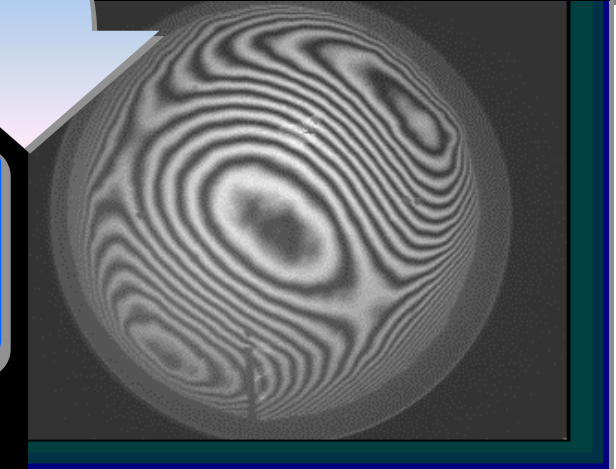
Stressed Mirror Polishing (SMP)



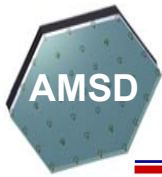
Finishing the R2 Surface



Metrology



*Optical fabrication by  
Stressed Mirror Polishing (SMP).*



# Optical Fabrication: Tooling for Water Jet Milling



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Cutting the mask  
by water jet



Completed mask



Isogrid blocking body



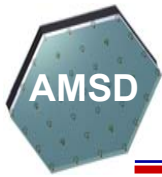
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Mask positioned on  
Facesheet/blocking body



***Preparing the tooling for  
water jet light-weighting.***

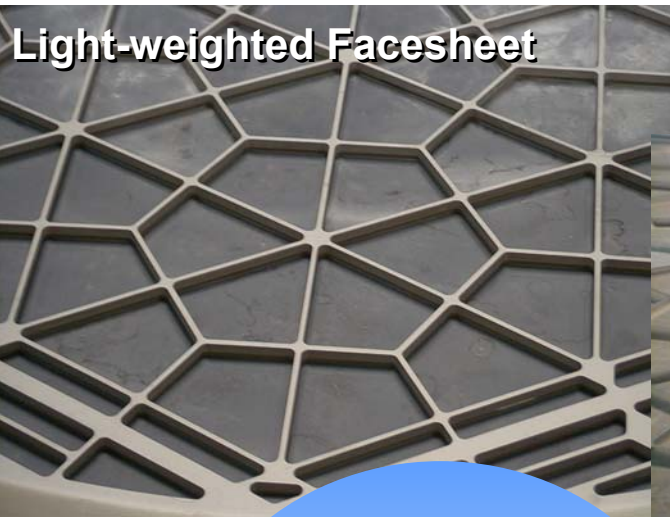




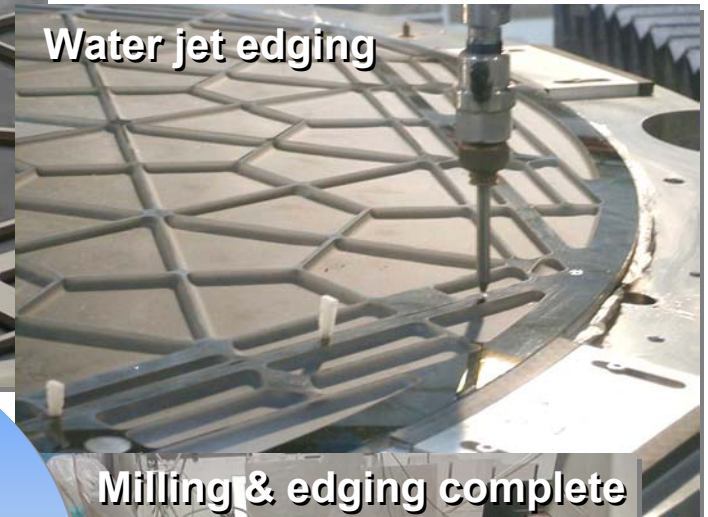
# Optical Fabrication: Light-Weighting and Edging



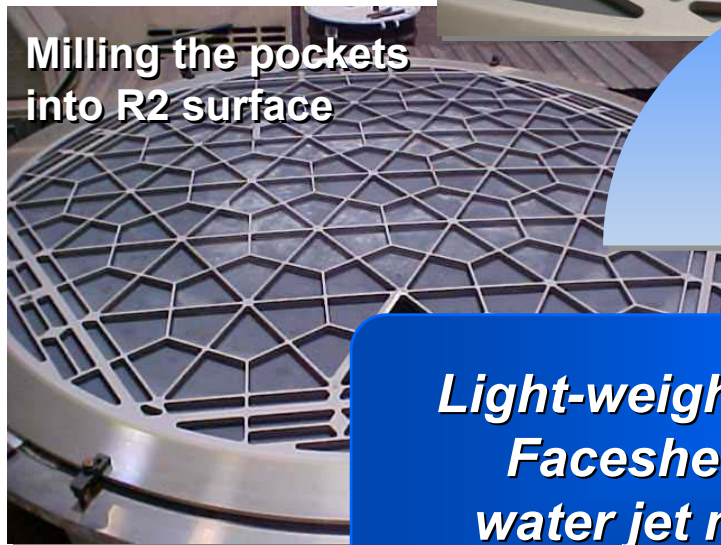
VG H26-0068 21



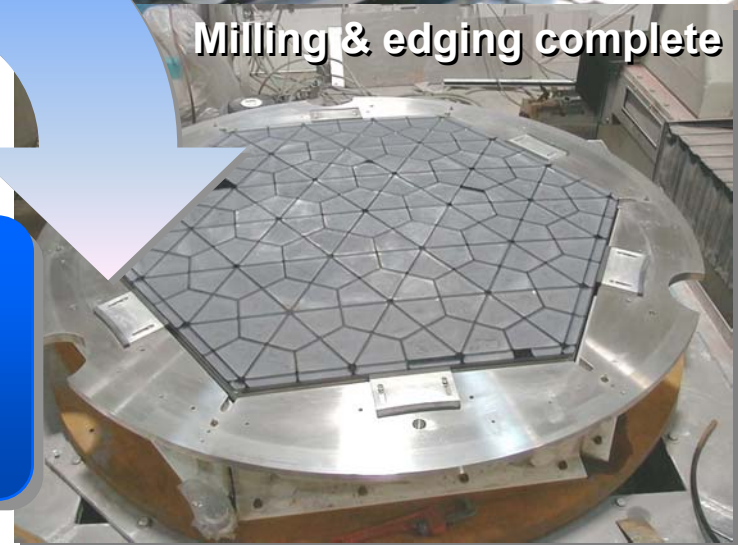
Light-weighted Facesheet



Water jet edging

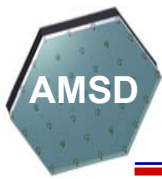


Milling the pockets  
into R2 surface



Milling & edging complete

*Light-weighting the  
Facesheet by  
water jet milling.*



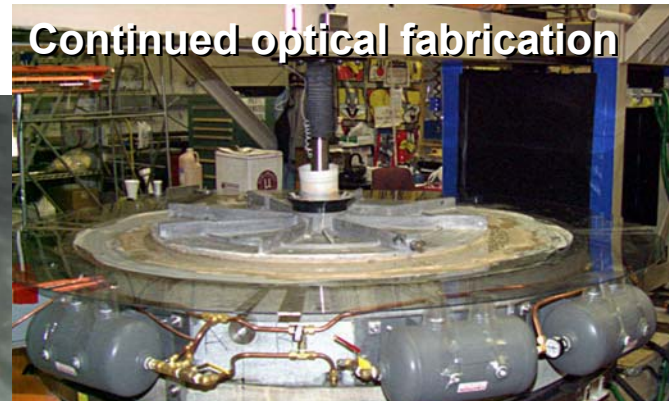
# Optical Fabrication: Fracture and Recovery



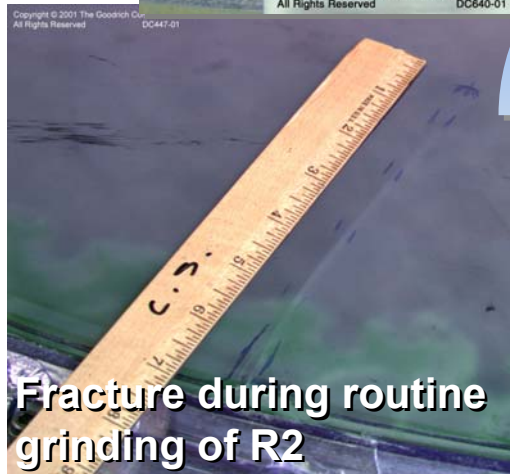
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Fracture "repair"



Continued optical fabrication

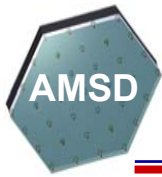


Fracture during routine grinding of R2



Repair area excised during edging

***Optical fabrication completed as planned;  
no loss of actuators.***

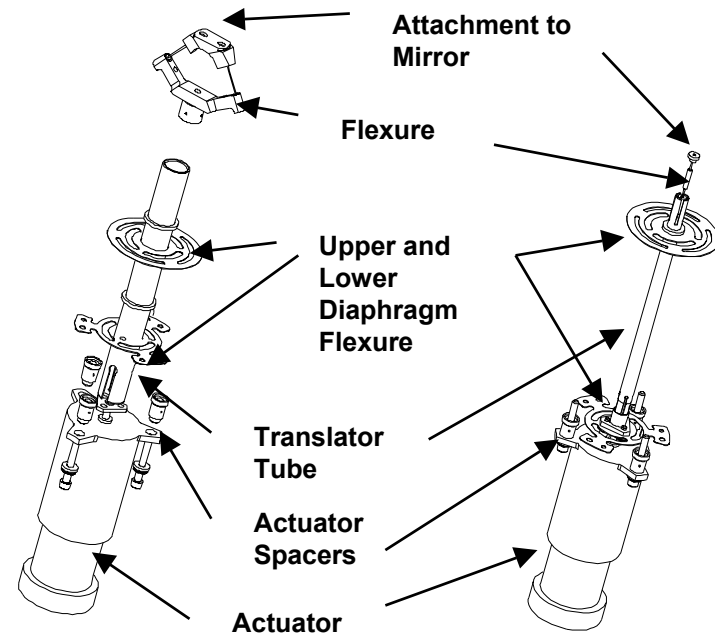


- **Facesheet Progress and Status:**
  - Fracture “repair” complete
  - Optical fabrication by SMP complete
  - Light-weighting by water jet milling complete
  - Edging by water jet complete
  - Beveling and stress relief in progress
  - Preparations for Facesheet Subassembly underway

***Optical fabrication complete;  
Stressed Mirror Polishing advantages demonstrated.***

## Actuators and Controller:

- Design overview
- Controller
- Test results
- Status

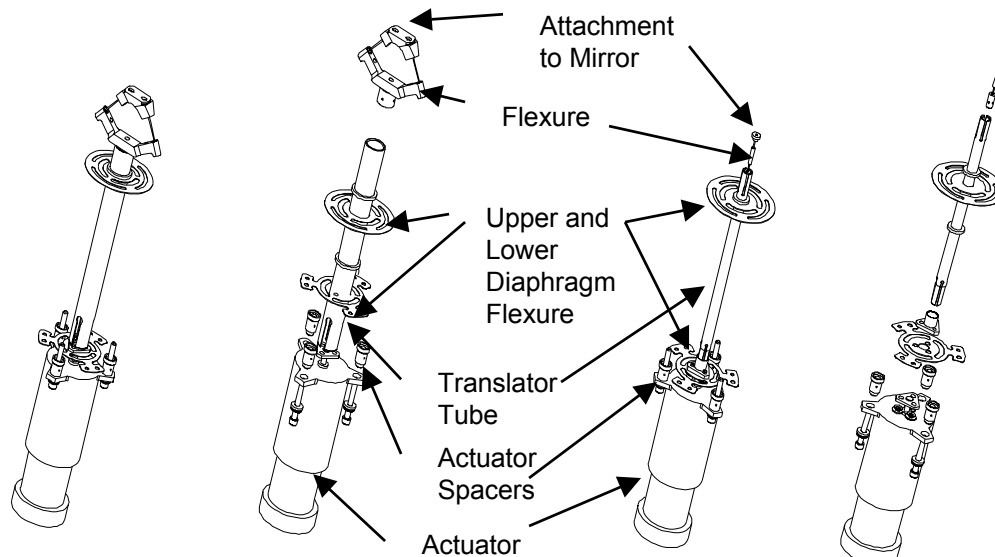


Bipod Assembly

Axial Assembly

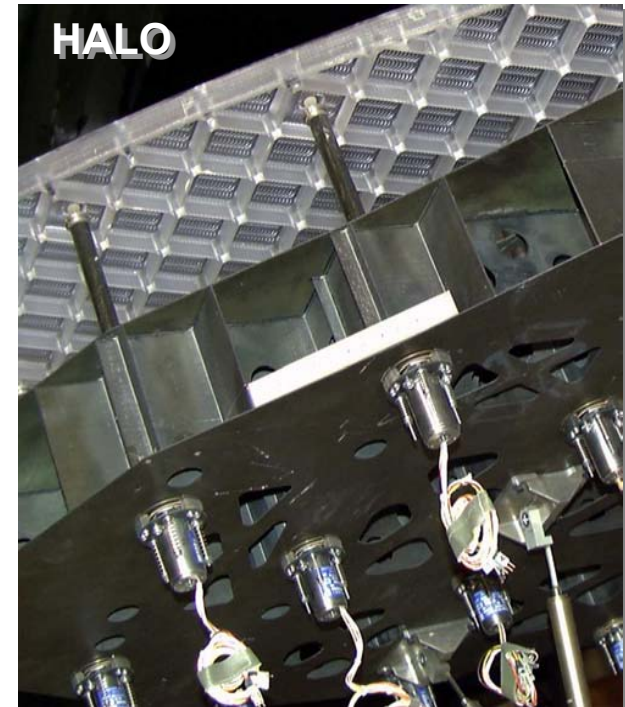


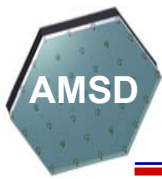
- **Actuator assemblies (6 “Bipod”, 31 “Axial”) react all loads**
- **Similar to HALO (also cryogenic)**
- **Upper and lower diaphragm flexures stabilize translator & flexure, provide shear and moment load path for bipods**
- **Allows easy access to actuators for installation and servicing**



**Bipod Assembly**

**Axial Assembly**



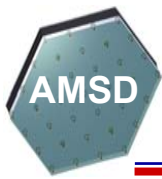


# Actuator Design Parameters Summary

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Performance Parameter	Reason
Stroke	Ground test and post-deployment capture range
Resolution	Performance (quantization)
Mass	Observatory flow-down
Reliability and Lifetime	Maintain low performance risk
Room and Cryogenic Performance	Operational performance and efficient ground-test strategy
Low (zero) Power Dissipation	Thermal maintenance Operational efficiency
Axial Stiffness	PMA Dynamics
Compatibility with Cryo-Appropriate Command/Power Structure	Minimize wire count for deployment Maintain reliability and redundancy

- **Goodrich has selected stepper-motor based actuator from Moog-Shaeffer Magnetics Division (SMD):**
  - Derived from NASA-funded cryo actuator studies
  - Engineered under Goodrich and Moog IRAD



# Actuator Design: Space Rated Materials for Cryogenic Operation



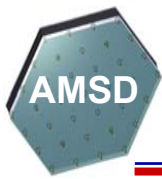
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Titanium Alloy (6AL-4V)	General Construction: Housing/Transducer, Motor Housing, Thrust Rod, Spring/Nut Element, Output Flange
Stainless Steel (440C)	Bearings, Harmonic Drive Wave Generator
Stainless Steel (Nitronic40)	Output Leadscrew
Stainless Steel (15-5PH)	Harmonic Drive Circular Spline and Flex Spline
Stainless Steel (416)	Motor Rotor

- **Actuator internal bearings, harmonic drive wave generator, lead screw/nut use dry lubricant for low room temperature friction and excellent molecular bonding**
- **Materials are selected specifically for cryogenic application and compatibility**
- **Structural members are sized to perform over life with ample margin**
- **Fasteners are generally titanium with only a few 416 stainless steel (thermally matched)**

***Performance demonstrated at 30K,  
consistent with AMSD requirements.***

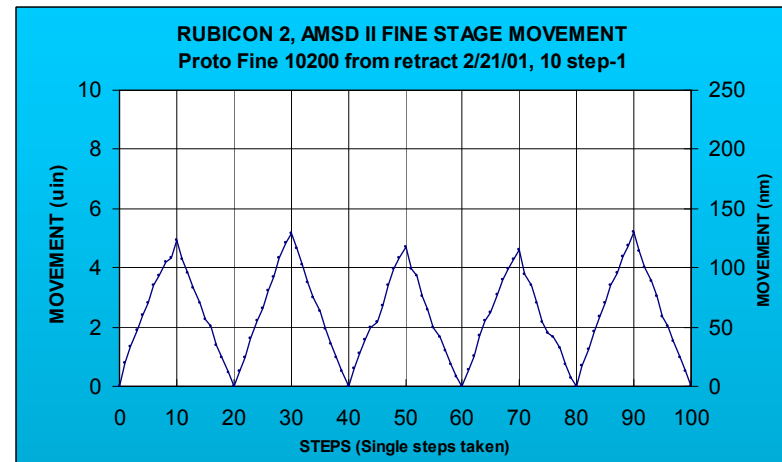
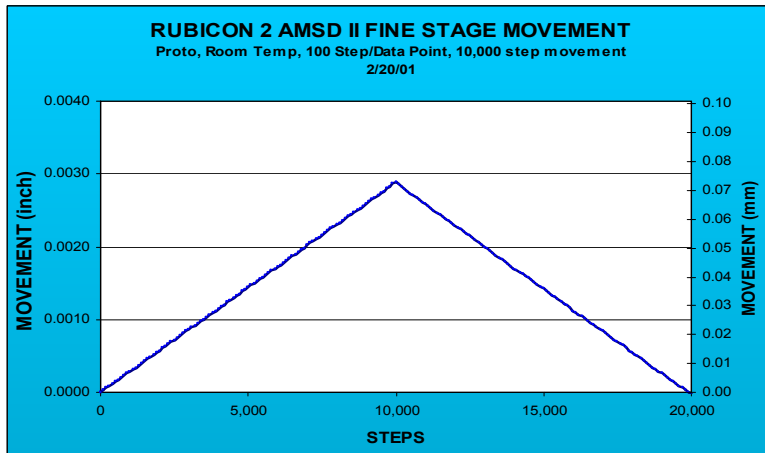


# Actuator Design Verified at RT and Cryo



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Room temperature tests:



## Example Data:

- Average Step Size = 7.3 nanometers
- Standard Deviation = 3.5 nanometers
- Meets requirement for max. step size < 20 nanometers

## RT vs. Cryo Performance:

- Same general behavior when unloaded
- Some units have exhibited anomalous behavior under load at cryo
- More extensive cryo tests underway



# Actuator Electronics: Design Requirements



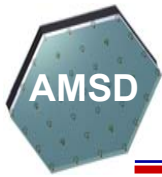
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- **Architecture must be traceable to deployable, space-borne applications**
- **Minimize wire-count between nodes and central controller**
  - Hold actuator position with minimal actuator power
  - Minimize overall power dissipation
- **Architecture must be scaleable to large arrays of actuators**
- **Circuit design must be traceable to operation at 30K**
  - Operate over temperature range from 30 to 293K
  - Active devices MOS (bipolar processes freeze-out at  $T < \sim 70K$ )
- **AMSD Electronics design does not limit bandwidth ( $\approx 0.1$  Hz update rate)**

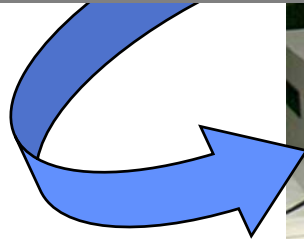
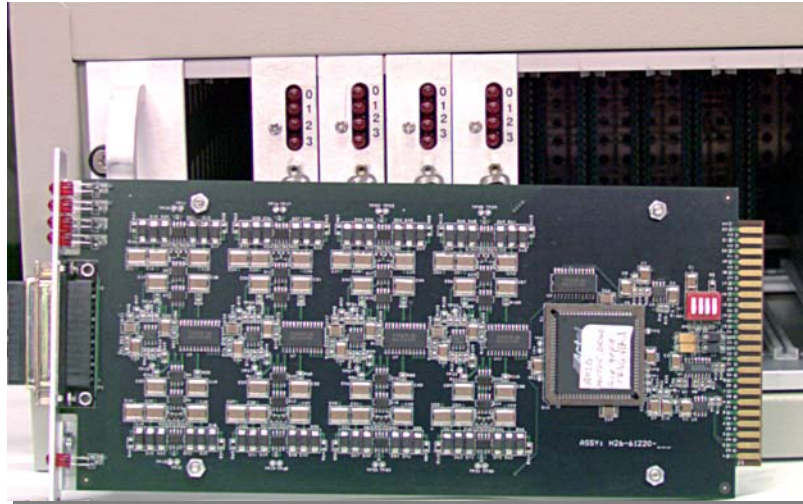


- **Control Computer (CC) and array of actuator nodes form “ring”**
  - Serial communication minimizes wire count
  - Resistive isolation between nodes prevents fault propagation
  - Easily provides required throughput
  - Ultimate bandwidth limit is motor dynamics
- **All system “intelligence” in software executing on CC**
  - Directly commands motor windings to desired states
  - Operationally flexible, upgradeable
- **“Dumb” hardware at nodes**
  - Translate winding state commands to winding drive currents
  - Minimizes hardware complexity, maximizes system flexibility
- **Topology is inherently scalable**
  - Change CC software required
- **AMSD drive electronics are “warm”  
(located outside vacuum chamber)**





## AMSD 4-channel Actuator Driver Circuit Card



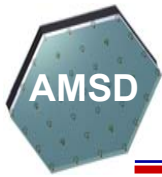
***Drive electronics, controller,  
software and cabling are complete.***



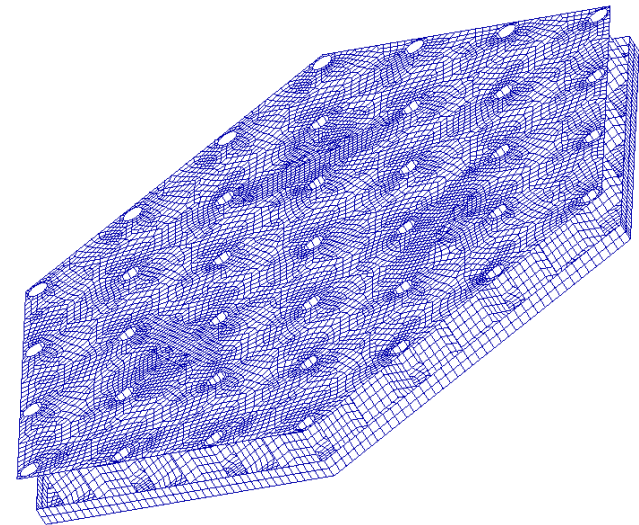
- **Actuators/Controller Progress and Status:**
  - All 37 AMSD units have been delivered
  - Drive electronics and controller complete
  - Performance tests at RT complete
  - More extensive cryo testing under load underway
  - Integration of actuation components with Reaction Structure underway

***All actuators delivered;  
basic design/performance verified.***

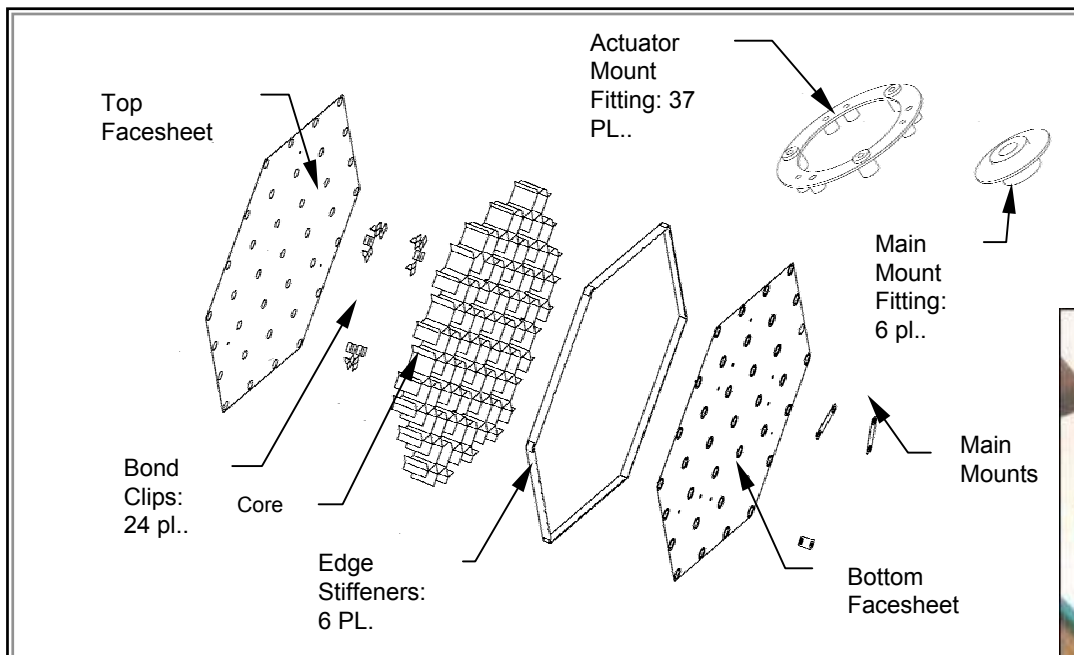




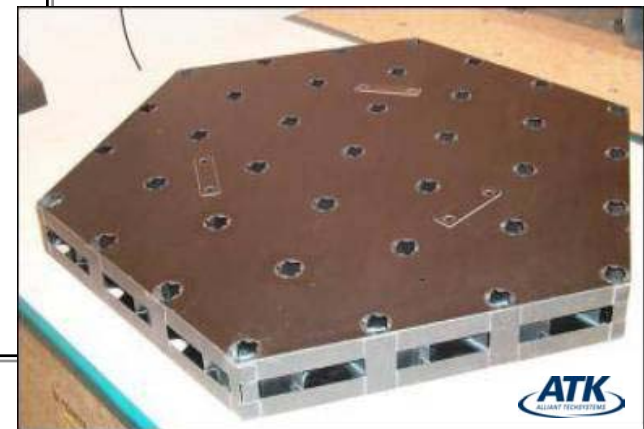
- **Composite Reaction Structure:**
  - Design and construction
  - Modeling
  - Delamination and repair
  - Cryo test results
  - Status

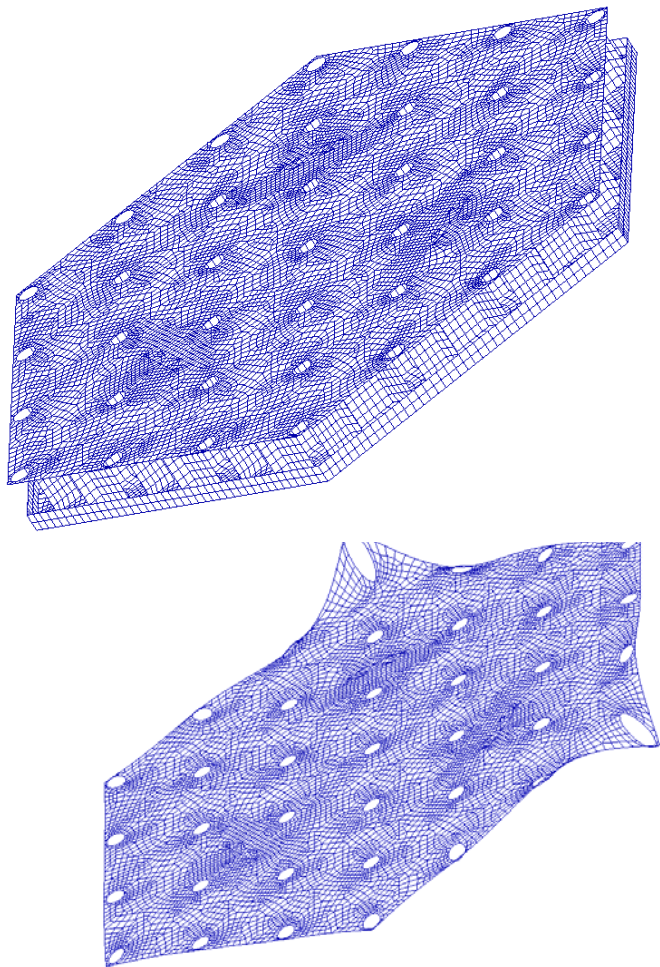
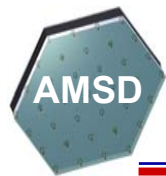


- Graphite cyanate-ester for CTE match with glass Facesheet
- Mounts actuators and flexures; reacts loads from masses and figuring
- Interfaces to external mount
- Designed and manufactured by ATK

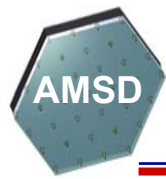


*Photo of completed unit*





- **NASTRAN Detailed Finite Element Model**
  - Layered shell elements
  - 37 concentrated mass elements representing actuators and INVAR fittings
  - Simple support at main mount locations
- **Predicted response of baseline structure meets requirement (1st mode reduced to due to repair)**

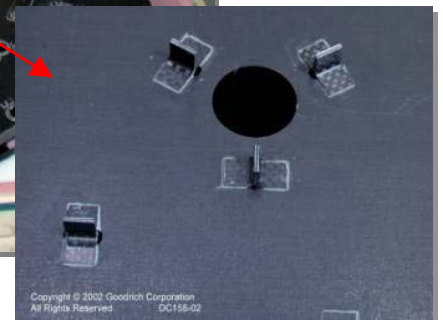
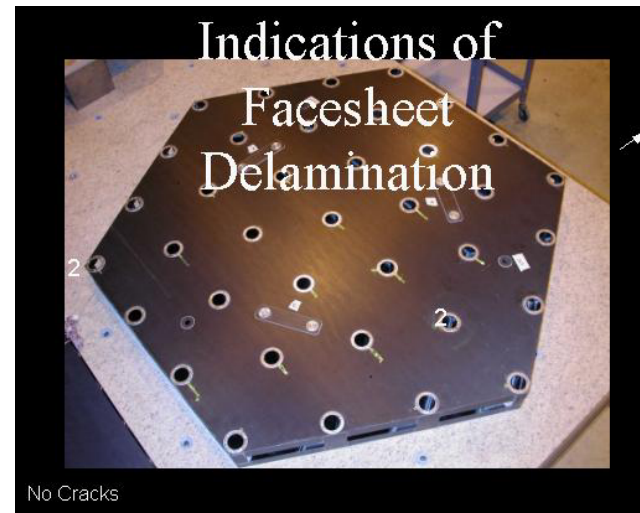


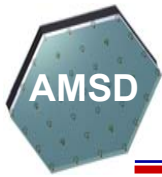
# CRS: Delamination and Repair



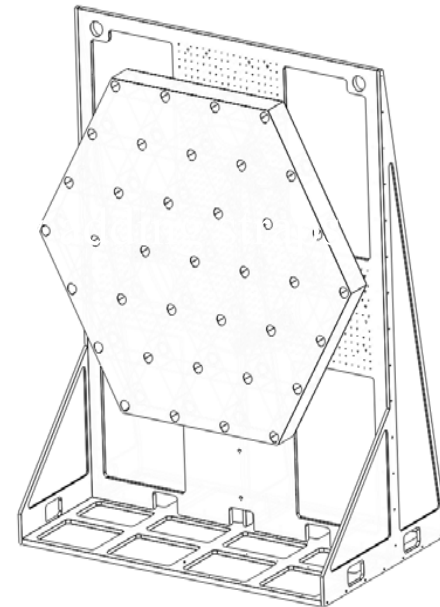
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- **Post cryo cycling inspection revealed voids in facesheets:**
  - Voids at specific orientation over core ribs
  - Attributed to alignment of facesheet plies relative to core cells
- **Repaired by composite straps between top and bottom facesheets:**
  - At every location of actual or likely delamination
  - Repair complete
  - CRS cryo cycled at the XRCF
- **Origin of failure and solutions identified**



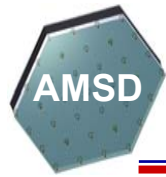


- **Tests conducted on repaired CRS:**
  - **Thermal cycle to 25 K at XRCF**
    - No metrology for distortion
    - No further delamination
  - **10-G static load test at ATK**
  - **Thermal characterization at XRCF**
    - Instrumented for distortion measurements
    - Two cycles to 25 K
    - Measured distortion within acceptable limits



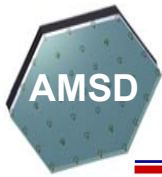
CRS on cryo test stand at XRCF





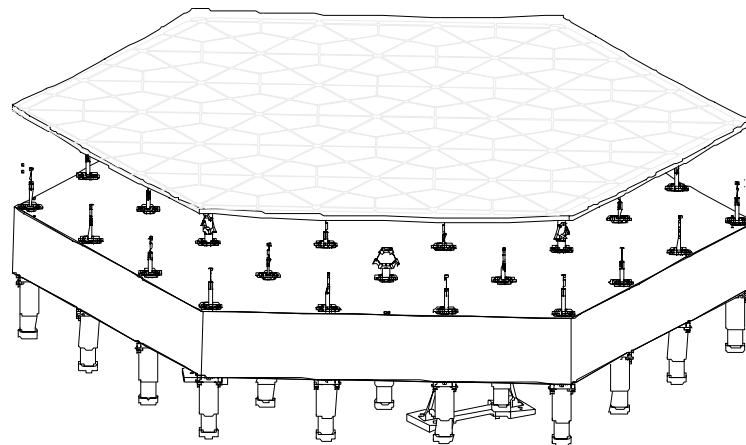
- **CRS Progress and Status:**
  - **Fabrication complete**
  - **Delamination:**
    - Causes and solutions identified
    - Repair complete
  - **Cryo test of repaired unit complete**
  - **Integration with actuation system underway**

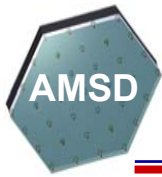
***CRS complete and verified by  
analysis and measurement.***



- **Assembly and Integration:**

- Assembly description
- Integration process
- Status and Plans

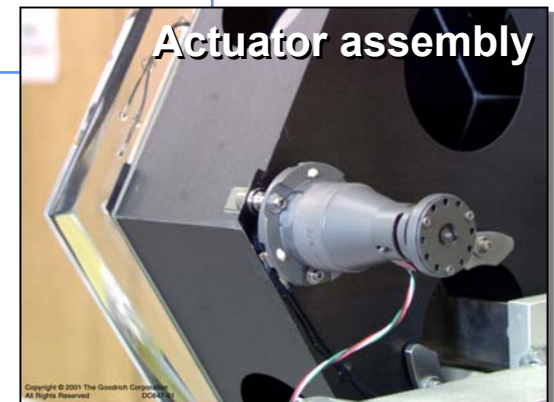
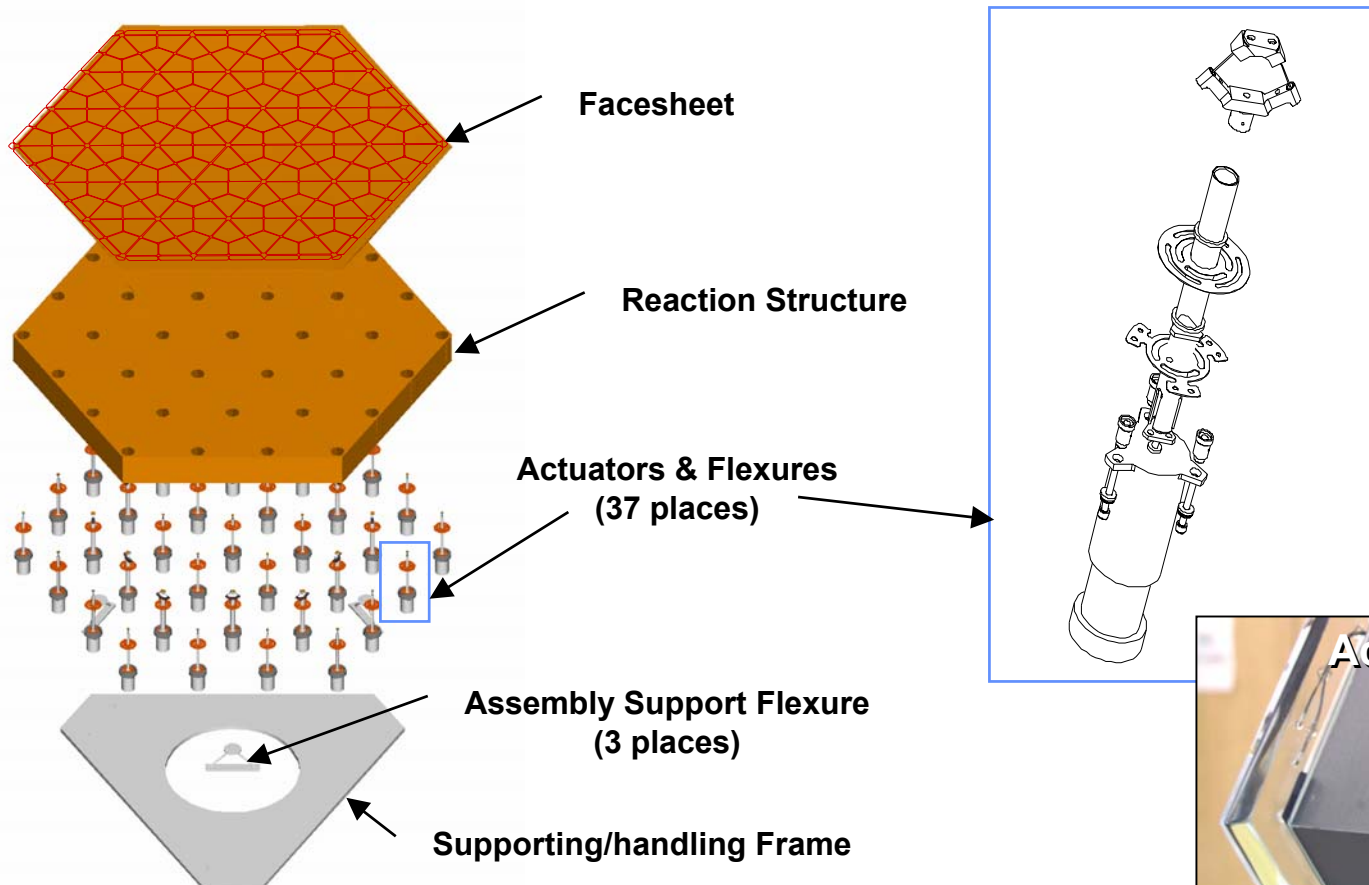




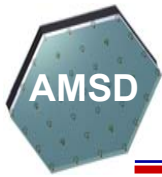
# Assembly Description



VG H26-0068 40



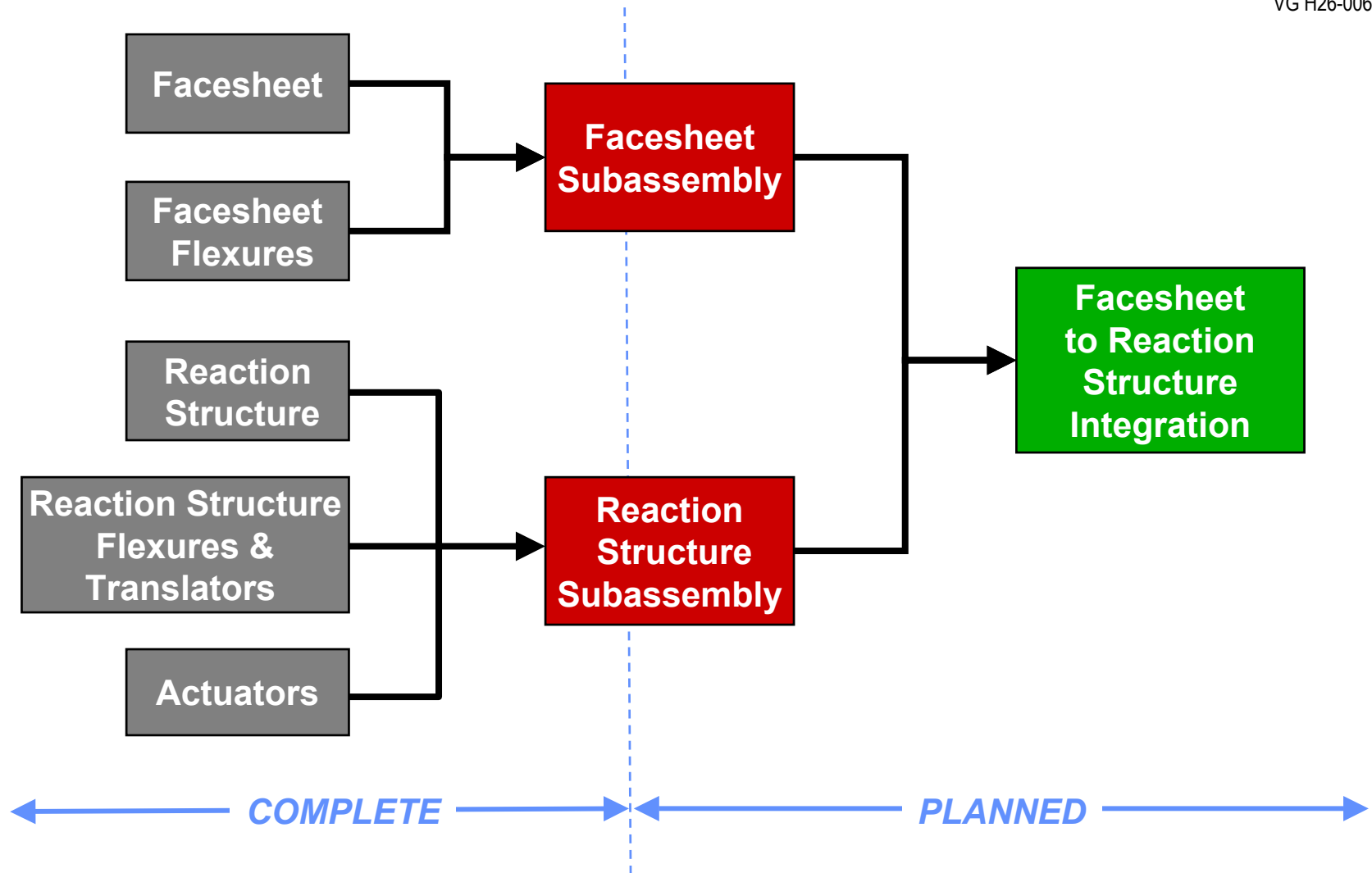


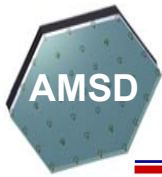


# Hardware Integration Flow



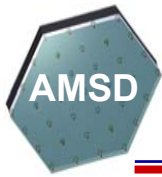
VG H26-0068 41



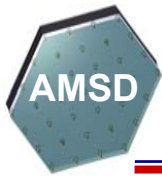


- **Assembly and Integration Progress and Status:**
  - Design and process definition complete
  - Tooling design and fabrication partly complete and continuing
  - Reaction Structure/Actuator subassembly in progress
  - Preparations for Facesheet Subassembly underway

***Assembly and Integration in progress per plan.***



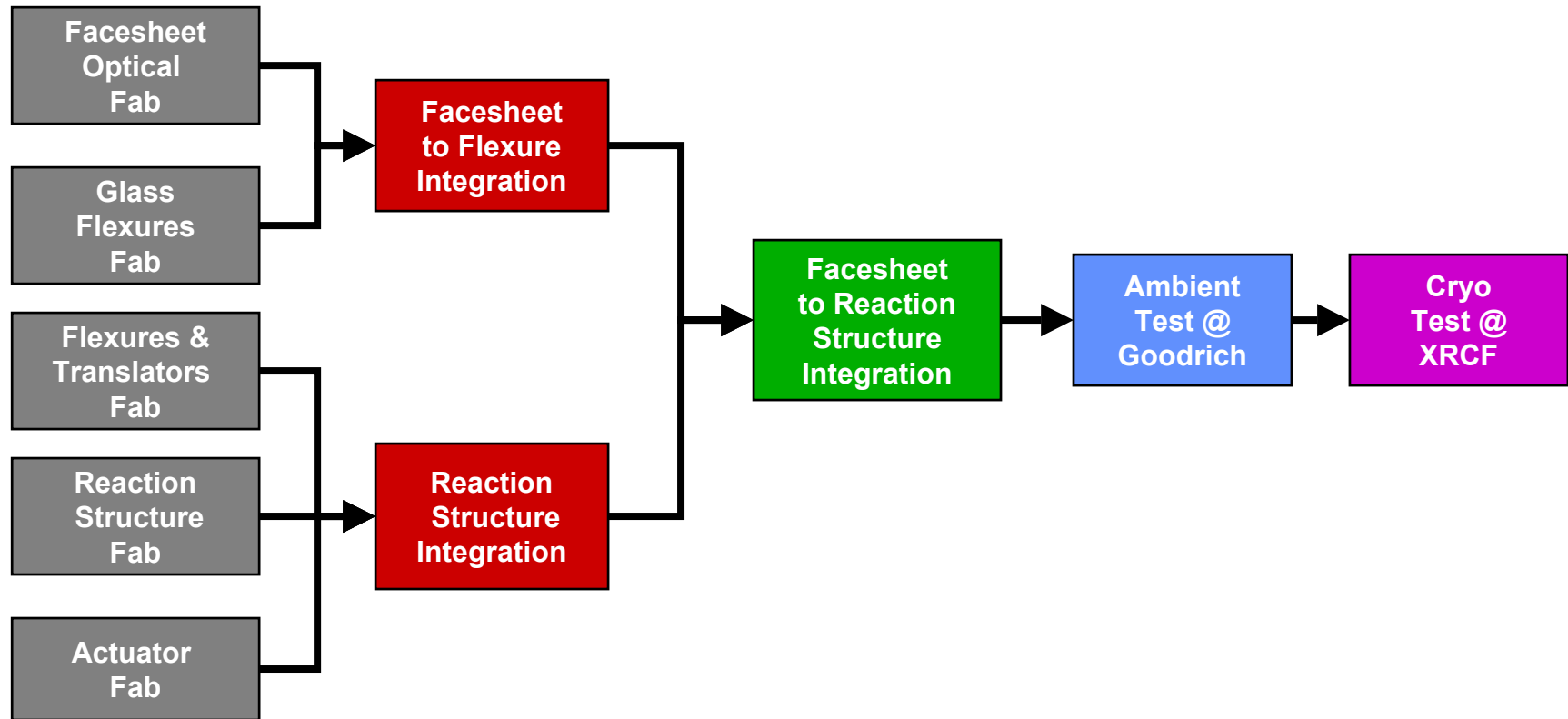
- Program Objectives and Requirements
- Goodrich Configuration Overview
- Progress Update and Status
  - Facesheet
  - Actuators and Controller
  - Reaction Structure
  - Assembly and Integration
- **Test Plan and Program Schedule**
- Summary and Conclusions

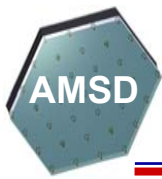


# Process Flow Summary



VG H26-0068 44

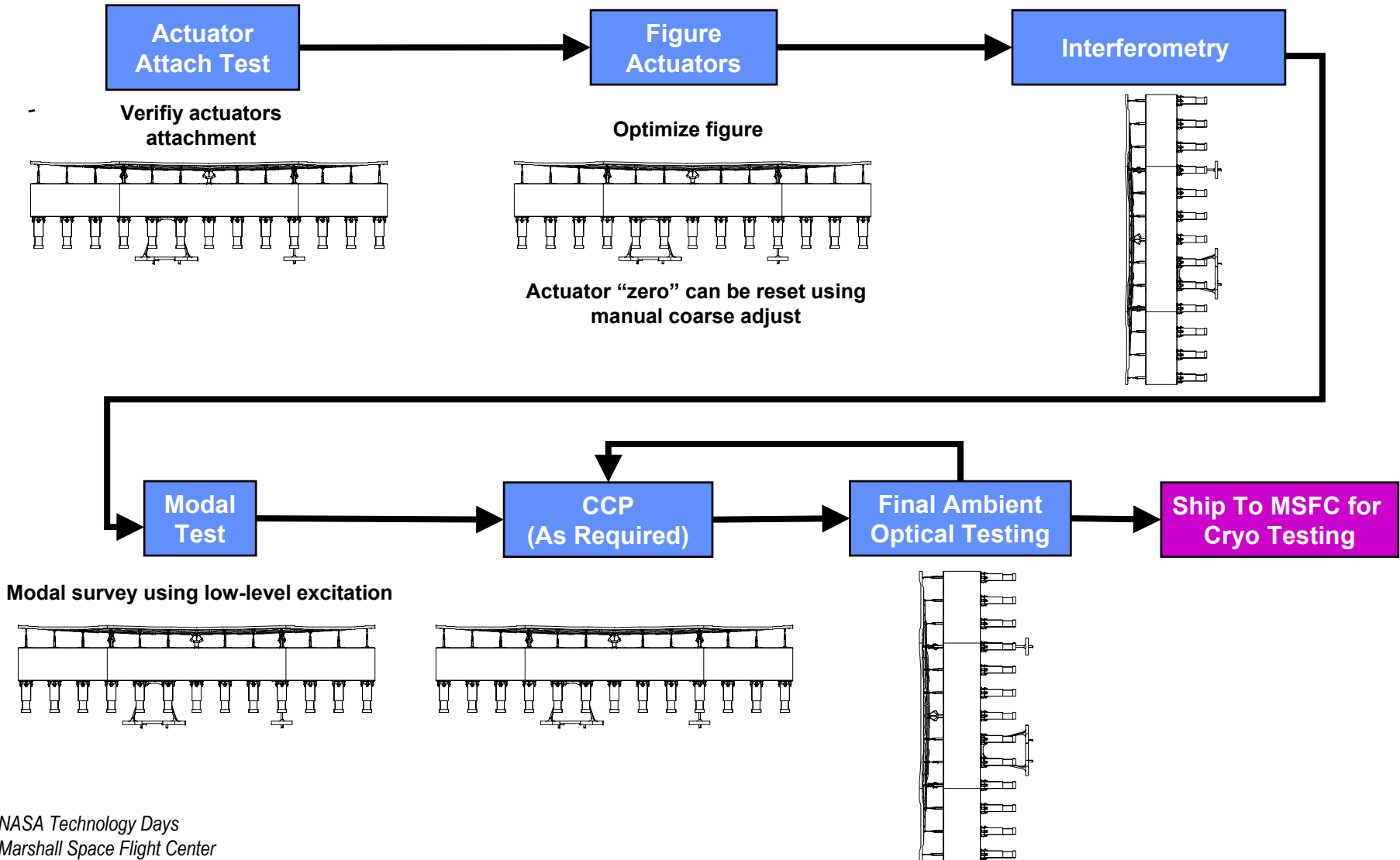


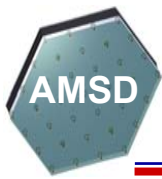


# Test & Verification (RT at Goodrich)



VG H26-0068 45

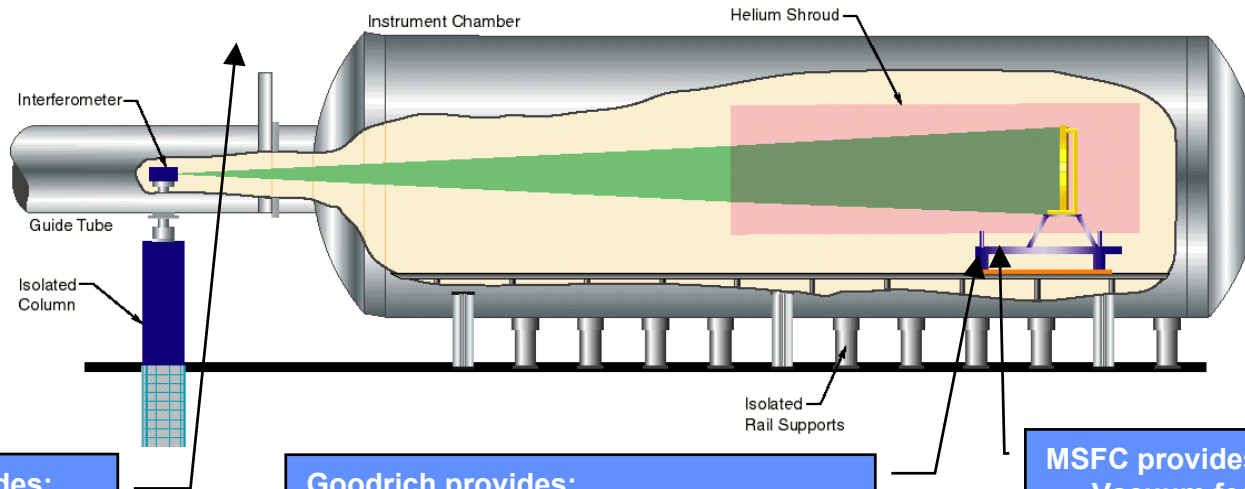




# Cryo Test Arrangements at the XRCF



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## MSFC provides:

- Interferometer
- Objective Lens
- Leica ADM
- Window
- DNC

## Goodrich provides:

- In-chamber cabling for actuators & temp. sensors
- Out-chamber cabling for actuators
- Mirror Assembly temp. sensors
- Actuator Control Electronics & PC

## MSFC provides:

- Vacuum feedthroughs
- Cabling to control room
- Temp. sensor's readouts
- 5 DOF positioning table

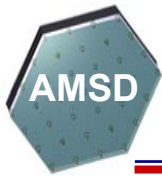
- Establish ambient baseline alignment
- Measure ambient baseline figure

Partially cool chamber

- Measure figure
- Adjust figure actuators as required to minimize figure error
- Track actuator and despace changes over temperature range

- Measure figure at cryogenic operating temperature





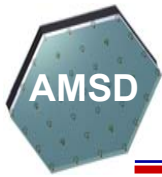
# Agenda



VG H26-0068 48

- Program Objectives and Requirements
- Goodrich Configuration Overview
- Progress Update and Status
  - Facesheet
  - Actuators and Controller
  - Reaction Structure
  - Assembly and Integration
- Test Plan and Program Schedule
- **Summary and Conclusions**





- **Our AMSD design is traceable to operational systems:**
  - **Flexible facesheet** *enables efficient figuring of a readily produced substrate*
  - **‘Displacement’ type actuators** *stiffen facesheet against reaction structure while providing shape control*
  - **Reaction structure** *utilizes a high stiffness-to-mass material that is amenable to efficient structural forms*
  - **Material choices** *can be tailored to specific applications (facesheet and/or reaction structure)*
  - **‘External’ actuator** *permits adoption of improved designs*
  - **Mass and stiffness changes** *are addressed without disruption to key facesheet/actuator design and manufacturing details*

***Our AMSD design is fully traceable against the SOW requirements.***



- **Goodrich's AMSD architecture provides robust accommodation for a broad range of system and mission requirements:**
  - Readily accommodates alternative petal geometries
  - Readily accommodates alternative materials
  - Provides opportunity to trade mass, stiffness, and segment size for optimal mission responsiveness
  - Manufacturing technique is cost/schedule effective for multiple builds

***Rapid optical fabrication and isogriding have validated the recurring benefits of the AMSD manufacturing processes.***

